

### Unit: 3

Maxwell's Thermodynamic Relations: Derivation of Maxwell's Relations. Application of Maxwell's relation to (1) Clausius Clapeyron equation, (2) Values of  $C_p - C_v$ . (3) Tds equations, (4) Joule-Kelvin coefficient for ideal and Vander Waal gases, (5) Change of temperature during Adiabatic process etc.

Phase Transition: First and second order phase transition with examples, Clausius Clapeyron Equation.

Derivation of Maxwell's Thermodynamic relation: 21/09/24.

From the first law of thermodynamics, we have -

$$dQ = du + PdV$$

$$\Rightarrow du = dQ - PdV$$

Again, from second law of thermodynamics, we have -

$$dQ = Tds$$

$$\therefore du = Tds - PdV \quad \text{--- (1)}$$

Let,  $u, s$  and  $v$  be the function of 2 independent variable  $x$  and  $y$  then -

$$du = \left(\frac{\partial u}{\partial x}\right)_y dx + \left(\frac{\partial u}{\partial y}\right)_x dy$$

$$ds = \left(\frac{\partial s}{\partial x}\right)_y dx + \left(\frac{\partial s}{\partial y}\right)_x dy$$

$$dv = \left(\frac{\partial v}{\partial x}\right)_y dx + \left(\frac{\partial v}{\partial y}\right)_x dy$$

Putting the value of  $du, ds$  and  $dv$  in eq<sup>n</sup> (1), we get  $\Rightarrow$

$$\left(\frac{\partial u}{\partial x}\right)_y dx + \left(\frac{\partial u}{\partial y}\right)_x dy = T \left\{ \left(\frac{\partial s}{\partial x}\right)_y dx + \left(\frac{\partial s}{\partial y}\right)_x dy \right\} - P \left\{ \left(\frac{\partial v}{\partial x}\right)_y dx + \left(\frac{\partial v}{\partial y}\right)_x dy \right\}$$

$$\Rightarrow \left(\frac{\partial u}{\partial x}\right)_y dx + \left(\frac{\partial u}{\partial y}\right)_x dy = \left\{ T \left(\frac{\partial s}{\partial x}\right)_y - P \left(\frac{\partial v}{\partial x}\right)_y \right\} dx + \left\{ T \left(\frac{\partial s}{\partial y}\right)_x - P \left(\frac{\partial v}{\partial y}\right)_x \right\} dy$$

Equating the coefficient of  $dx$  and  $dy$ , we get  $\Rightarrow$

$$\left(\frac{\partial u}{\partial x}\right)_y = T \left(\frac{\partial s}{\partial x}\right)_y - P \left(\frac{\partial v}{\partial x}\right)_y \quad \text{--- (2)}$$

$$\left(\frac{\partial u}{\partial y}\right)_x = T \left(\frac{\partial s}{\partial y}\right)_x - P \left(\frac{\partial v}{\partial y}\right)_x \quad \text{--- (3)}$$

Differentiating eq<sup>n</sup> (2) wrt 'y' and eq<sup>n</sup> (3) wrt 'x', we get  $\Rightarrow$

$$\frac{\partial^2 u}{\partial x \partial y} = \left(\frac{\partial T}{\partial y}\right)_x \left(\frac{\partial s}{\partial x}\right)_y + T \left(\frac{\partial^2 s}{\partial x \partial y}\right) - \left(\frac{\partial P}{\partial y}\right)_x \left(\frac{\partial v}{\partial x}\right)_y - P \left(\frac{\partial^2 v}{\partial x \partial y}\right) \quad \text{--- (4)}$$

$$\frac{\partial^2 u}{\partial y \partial x} = \left(\frac{\partial T}{\partial x}\right)_y \left(\frac{\partial s}{\partial y}\right)_x + T \left(\frac{\partial^2 s}{\partial x \partial y}\right) - \left(\frac{\partial P}{\partial x}\right)_y \left(\frac{\partial v}{\partial y}\right)_x - P \left(\frac{\partial^2 v}{\partial x \partial y}\right) \quad \text{--- (5)}$$

since  $du$ ,  $ds$  and  $dv$  are perfect differentials.

$$\therefore \frac{\partial^2 u}{\partial x \partial y} = \frac{\partial^2 u}{\partial y \partial x} ; \frac{\partial T}{\partial y} = \frac{\partial T}{\partial x} \text{ and } \frac{\partial P}{\partial x} = \frac{\partial P}{\partial y}$$

$\Rightarrow$  So, from eq<sup>n</sup> (4) and eq<sup>n</sup> (5), we get  $\Rightarrow$

$$\left(\frac{\partial T}{\partial y}\right)_x \left(\frac{\partial s}{\partial x}\right)_y + T \left(\frac{\partial^2 s}{\partial x \partial y}\right) - \left(\frac{\partial P}{\partial y}\right)_x \left(\frac{\partial v}{\partial x}\right)_y - P \left(\frac{\partial^2 v}{\partial x \partial y}\right) = \left(\frac{\partial T}{\partial x}\right)_y \left(\frac{\partial s}{\partial y}\right)_x + T \left(\frac{\partial^2 s}{\partial x \partial y}\right) - \left(\frac{\partial P}{\partial x}\right)_y \left(\frac{\partial v}{\partial y}\right)_x - P \left(\frac{\partial^2 v}{\partial x \partial y}\right)$$



$$\Rightarrow \left[ \left( \frac{\partial T}{\partial x} \right)_y \left( \frac{\partial s}{\partial y} \right)_x - \left( \frac{\partial s}{\partial x} \right)_y \left( \frac{\partial T}{\partial y} \right)_x \right] = \left( \frac{\partial T}{\partial x} \right)_y \left( \frac{\partial s}{\partial y} \right)_x - \left( \frac{\partial s}{\partial x} \right)_y \left( \frac{\partial T}{\partial y} \right)_x \quad (b)$$

This is the general eq<sup>n</sup> for Maxwell's thermodynamic relation.

The different relation can be obtained by substituting the 4 variables,  $s, p, T$  and  $V$  for  $x$  and  $y$ .

1. First Relation: putting  $x = T$  and  $y = V$

$$\frac{\partial T}{\partial x} = 1 \quad ; \quad \frac{\partial V}{\partial x} = 0$$

$$\frac{\partial T}{\partial y} = 0 \quad ; \quad \frac{\partial V}{\partial y} = 1$$

$$\therefore \left( \frac{\partial T}{\partial V} \right)_T \left( \frac{\partial s}{\partial T} \right)_V - \left( \frac{\partial p}{\partial V} \right)_T \left( \frac{\partial T}{\partial T} \right)_V = \left( \frac{\partial T}{\partial T} \right)_V \left( \frac{\partial s}{\partial V} \right)_T - \left( \frac{\partial p}{\partial T} \right)_V \left( \frac{\partial V}{\partial V} \right)_T$$

$$\Rightarrow \left[ \left( \frac{\partial s}{\partial V} \right)_T = \left( \frac{\partial p}{\partial T} \right)_V \right]$$

2. Second Relation: putting  $x = T$  and  $y = P$

$$\frac{\partial T}{\partial x} = 1 \quad ; \quad \frac{\partial P}{\partial x} = 0$$

$$\frac{\partial T}{\partial y} = 0 \quad ; \quad \frac{\partial P}{\partial y} = 1$$

$$\left( \frac{\partial T}{\partial P} \right)_T \left( \frac{\partial s}{\partial T} \right)_P - \left( \frac{\partial p}{\partial P} \right)_T \left( \frac{\partial T}{\partial T} \right)_P = \left( \frac{\partial T}{\partial T} \right)_P \left( \frac{\partial s}{\partial P} \right)_T - \left( \frac{\partial p}{\partial T} \right)_P \left( \frac{\partial P}{\partial P} \right)_T$$

$$\Rightarrow - \left( \frac{\partial V}{\partial T} \right)_P = \left( \frac{\partial s}{\partial P} \right)_T$$

$$\Rightarrow \left[ \left( \frac{\partial s}{\partial P} \right)_T = - \left( \frac{\partial V}{\partial T} \right)_P \right]$$

3. Third Relation: Putting  $x=S$  ;  $y=V$

$$\frac{\partial S}{\partial x} = 1 \quad ; \quad \frac{\partial S}{\partial y} = 0$$

$$\frac{\partial V}{\partial x} = 0 \quad ; \quad \frac{\partial V}{\partial y} = 1$$

$$\text{Eq}^n(b) \Rightarrow \left( \frac{\partial T}{\partial V} \right)_S \cdot 1 - \left( \frac{\partial P}{\partial V} \right)_S \cdot 0 = \left( \frac{\partial T}{\partial S} \right)_V \cdot 0 - \left( \frac{\partial P}{\partial S} \right)_V \cdot 1$$

$$\Rightarrow \boxed{\left( \frac{\partial T}{\partial V} \right)_S = - \left( \frac{\partial P}{\partial S} \right)_V}$$

4. Fourth Relation: putting  $x=S$  ;  $y=P$

$$\frac{\partial S}{\partial x} = 1 \quad ; \quad \frac{\partial P}{\partial x} = 0$$

$$\frac{\partial S}{\partial y} = 0 \quad ; \quad \frac{\partial P}{\partial y} = 1$$

$$\text{Eq}^n(b) \Rightarrow \left( \frac{\partial T}{\partial P} \right)_S \left( \frac{\partial S}{\partial S} \right)_P - \left( \frac{\partial P}{\partial P} \right)_S \left( \frac{\partial V}{\partial S} \right)_P = \left( \frac{\partial T}{\partial S} \right)_P \left( \frac{\partial S}{\partial P} \right)_S - \left( \frac{\partial P}{\partial S} \right)_P \left( \frac{\partial V}{\partial P} \right)_S$$

$$\Rightarrow \left( \frac{\partial T}{\partial P} \right)_S - \left( \frac{\partial V}{\partial S} \right)_P = 0$$

$$\Rightarrow \boxed{\left( \frac{\partial T}{\partial P} \right)_S = \left( \frac{\partial V}{\partial S} \right)_P}$$

Application of Maxwell's Thermodynamic Relation:

1. Prove that  $\left( \frac{\partial Q}{\partial P} \right)_T = -T \left( \frac{\partial V}{\partial T} \right)_P = -TV\alpha$  where

the symbols have their usual meaning.

↳ From, Maxwell's relation, we have -

$$\left( \frac{\partial S}{\partial P} \right)_T = - \left( \frac{\partial V}{\partial T} \right)_P$$

→

$$\left(\frac{\partial S}{\partial P}\right)_T = -\left(\frac{\partial V}{\partial T}\right)_P$$

Multiplying both sides by  $T$ , we get  $\Rightarrow$

$$T \left(\frac{\partial S}{\partial P}\right)_T = -T \left(\frac{\partial V}{\partial T}\right)_P$$

$$\Rightarrow \left\{ \frac{\partial}{\partial P} (TS) \right\}_T = -T \left(\frac{\partial V}{\partial T}\right)_P$$

$$\Rightarrow \boxed{\left(\frac{\partial Q}{\partial P}\right)_T = -T \left(\frac{\partial V}{\partial T}\right)_P} \quad \text{--- (1)} ; \quad \boxed{Q = TS}$$

Now, from the definition of coefficient of volume expansion, we have -

$$\alpha = \frac{1}{V} \left(\frac{\partial V}{\partial T}\right)_P$$

$$\Rightarrow V\alpha = \left(\frac{\partial V}{\partial T}\right)_P$$

$$\therefore \text{Eq}^n (1) \Rightarrow \boxed{\left(\frac{\partial Q}{\partial P}\right)_T = -T \left(\frac{\partial V}{\partial T}\right)_P = -TV\alpha}$$

v2. show that -  $C_P - C_V = TE\alpha^2 V$ ; Where  $E$  is the bulk modulus of elasticity, and  $\alpha$  is the co-efficient of vol.<sup>m</sup> expansion.

$\hookrightarrow$  From the definition of specific heat <sup>at</sup> constant  $P$  and  $V$ , we have -

$$C_P = \left(\frac{\partial Q}{\partial T}\right)_P = T \left(\frac{\partial S}{\partial T}\right)_P$$

$$\text{and } C_V = \left(\frac{\partial Q}{\partial T}\right)_V = T \left(\frac{\partial S}{\partial T}\right)_V$$

since,  $dS$  is a perfect diff. wrt  $T$  and  $V$ , we can write  $\Rightarrow$

$\rightarrow$

$$ds = \left(\frac{\partial s}{\partial T}\right)_V dT + \left(\frac{\partial s}{\partial V}\right)_T dV$$

Differentiating wrt 'T' and at constant 'P', we get-

$$\left(\frac{\partial s}{\partial T}\right)_P = \left(\frac{\partial s}{\partial T}\right)_V + \left(\frac{\partial s}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_P$$

$$\Rightarrow T \left(\frac{\partial s}{\partial T}\right)_P = T \left(\frac{\partial s}{\partial T}\right)_V + T \left(\frac{\partial s}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_P$$

$$\Rightarrow T \left(\frac{\partial s}{\partial T}\right)_P - T \left(\frac{\partial s}{\partial T}\right)_V = T \left(\frac{\partial s}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_P$$

$$\Rightarrow C_p - C_v = T \left(\frac{\partial s}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_P \quad \text{--- (1)}$$

Again, P is a function of 'V' and 'T' also dP is a perfect differentiation.

$$dP = \left(\frac{\partial P}{\partial T}\right)_V dT + \left(\frac{\partial P}{\partial V}\right)_T dV$$

If the process is isobaric then  $dP = 0$

$$\left(\frac{\partial P}{\partial T}\right)_V dT = - \left(\frac{\partial P}{\partial V}\right)_T dV$$

$$\Rightarrow \left(\frac{\partial P}{\partial T}\right)_V = - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_P \quad \text{--- (2)}$$

Also, from Maxwell's relation we have -

$$\left(\frac{\partial s}{\partial V}\right)_T = \left(\frac{\partial P}{\partial T}\right)_V \quad \text{--- (3)}$$

using eq<sup>n</sup> (2) and eq<sup>n</sup> (3) in eq<sup>n</sup> (1); we get  $\Rightarrow$

$$C_p - C_v = T \left\{ \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial V}{\partial T}\right)_P \right\} \quad \left[ \text{using eq<sup>n</sup> (3)} \right]$$

$$\Rightarrow C_p - C_v = T \left\{ - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_P \left(\frac{\partial V}{\partial T}\right)_P \right\} \quad \left[ \text{using eq<sup>n</sup> (2)} \right]$$

$$\Rightarrow C_p - C_v = -T \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_P^2 \quad \text{--- (4)}$$

from the definition of Bulk modulus -

$$E = - \left( \frac{\partial P}{\partial V/V} \right)_T$$

$$\Rightarrow E = -V \left( \frac{\partial P}{\partial V} \right)_T$$

$$\Rightarrow \left( \frac{\partial P}{\partial V} \right)_T = \frac{-E}{V} \quad \text{--- (5)}$$

Also from the definition of vol.<sup>m</sup> expansion, we have -

$$\alpha = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

$$\Rightarrow \alpha V = \left( \frac{\partial V}{\partial T} \right)_P \quad \text{--- (6)}$$

Using eq<sup>n</sup> (5) and eq<sup>n</sup> (6) in eq<sup>n</sup> (4), we get  $\Rightarrow$

$$C_p - C_v = -T \left( -\frac{E}{V} \right) (\alpha V)^2$$

$$\Rightarrow \boxed{C_p - C_v = TE\alpha^2 V} \quad \text{(Hence proved)}$$

### 3. Derivation of Clausius Clapeyron eq<sup>n</sup>:

From Maxwell's Thermodynamic relation we have -

$$\left( \frac{\partial S}{\partial V} \right)_T = \left( \frac{\partial P}{\partial T} \right)_V$$

$$\Rightarrow T \left( \frac{\partial S}{\partial V} \right)_T = T \left( \frac{\partial P}{\partial T} \right)_V$$

$$\Rightarrow \left( \frac{\partial Q}{\partial V} \right)_T = T \left( \frac{\partial P}{\partial T} \right)_V \quad \text{--- (1)} \quad \left[ \partial Q = T \partial S \right]$$

Here  $\left( \frac{\partial Q}{\partial V} \right)_T$  represent the quantity of heat absorb or liberated per unit vol.<sup>m</sup> at constant temperature. So this quantity of heat absorb or liberated at constant temperature must be the latent heat and change in vol.<sup>m</sup> must be due to change in heat.

$\rightarrow$

If we consider unit mass of a substance and  $L$  be the latent heat when the substance change in  $V$  in  $V_1$  and  $V_2$  at constant  $T$ , then -

$$\partial Q = L \quad \text{and} \quad \partial V = V_2 - V_1$$

So, Eq<sup>n</sup> (1) becomes  $\Rightarrow$

$$\left( \frac{L}{V_2 - V_1} \right)_T = T \left( \frac{\partial p}{\partial T} \right)_V$$

$$\Rightarrow \frac{L}{V_2 - V_1} = T \frac{dp}{dT}$$

$$\Rightarrow \boxed{\frac{dp}{dT} = \frac{L}{T(V_2 - V_1)}}$$

Which is Clausius - Clapeyron equation.

#### 4. Three Tds equation:

Depending on the choice of independent variable there are three Tds equation:

(a) First Tds equation: In this case we take  $T$  and  $V$  as independent variable of entropy  $S$ .

$$S = S(T, V)$$

$$\therefore dS = \left( \frac{\partial S}{\partial T} \right)_V dT + \left( \frac{\partial S}{\partial V} \right)_T dV$$

$$\Rightarrow T dS = T \left( \frac{\partial S}{\partial T} \right)_V dT + T \left( \frac{\partial S}{\partial V} \right)_T dV$$

$$\Rightarrow T dS = \left( \frac{\partial Q}{\partial T} \right)_V dT + T \left( \frac{\partial S}{\partial V} \right)_T dV$$

$$\Rightarrow T dS = C_V dT + T \left( \frac{\partial S}{\partial V} \right)_T dV$$

Using Maxwell's relation, we have -

$$\left( \frac{\partial S}{\partial V} \right)_T = \left( \frac{\partial p}{\partial T} \right)_V$$

$$\therefore Tds = C_v dT + T \left( \frac{\partial p}{\partial T} \right)_V dv \quad \text{--- (1)}$$

(b) Second Tds equation: In this case we take T and p as independent variable of entropy s.

$$s = s(T, p)$$

$$\therefore ds = \left( \frac{\partial s}{\partial T} \right)_p dT + \left( \frac{\partial s}{\partial p} \right)_T dp$$

$$\Rightarrow Tds = T \left( \frac{\partial s}{\partial T} \right)_p dT + T \left( \frac{\partial s}{\partial p} \right)_T dp$$

$$\Rightarrow Tds = \left( \frac{\partial Q}{\partial T} \right)_p dT + T \left( \frac{\partial s}{\partial p} \right)_T dp$$

$$\Rightarrow Tds = C_p dT + T \left( \frac{\partial s}{\partial p} \right)_T dp$$

Now from Maxwell relation -

$$\left( \frac{\partial s}{\partial p} \right)_T = - \left( \frac{\partial v}{\partial T} \right)_p$$

$$\therefore Tds = C_p dT - T \left( \frac{\partial v}{\partial T} \right)_p dp \quad \text{--- (2)}$$

Also,  $\alpha = \frac{1}{V} \left( \frac{\partial v}{\partial T} \right)_p$

$$\Rightarrow \left( \frac{\partial v}{\partial T} \right)_p = \alpha V$$

$\therefore$  Eq<sup>n</sup> (2) becomes  $\Rightarrow$

$$Tds = C_p dT - T \alpha V dp \quad \text{--- (3)}$$

(c) Third Tds equation: In this case p and v is independent variable of entropy s.

$$\therefore s = s(p, v)$$

$$\therefore ds = \left( \frac{\partial s}{\partial p} \right)_v dp + \left( \frac{\partial s}{\partial v} \right)_p dv$$

$$\Rightarrow Tds = T \left( \frac{\partial s}{\partial p} \right)_v dp + T \left( \frac{\partial s}{\partial v} \right)_p dv$$

→

$$\Rightarrow T ds = T \left\{ \left( \frac{\partial s}{\partial T} \right)_V \left( \frac{\partial T}{\partial P} \right)_V \right\} dP + T \left\{ \left( \frac{\partial s}{\partial T} \right)_P \left( \frac{\partial T}{\partial V} \right)_P \right\} dV$$

$$\Rightarrow T ds = \left( \frac{\partial Q}{\partial T} \right)_V \left( \frac{\partial T}{\partial P} \right)_V dP + \left( \frac{\partial Q}{\partial T} \right)_P \left( \frac{\partial T}{\partial V} \right)_P dV$$

$$\Rightarrow \boxed{T ds = C_V \left( \frac{\partial T}{\partial P} \right)_V dP + C_P \left( \frac{\partial T}{\partial V} \right)_P dV} \quad \text{--- (4)}$$

Importance: (To find the entropy of a substance from the directly measurable quantities).

vs. change of temperature during adiabatic process:

From Maxwell's thermodynamic relation, we have -

$$\left( \frac{\partial T}{\partial V} \right)_S = - \left( \frac{\partial P}{\partial S} \right)_V$$

$$\Rightarrow \left( \frac{\partial T}{\partial V} \right)_S = -T \left( \frac{\partial P}{\partial Q} \right)_V ; \quad \boxed{\partial Q = T \partial S}$$

Since increasing amount of heat at constant vol<sup>m</sup> always results in increase pressure  $\left( \frac{\partial P}{\partial Q} \right)_V$  is positive hence the form  $\left( \frac{\partial T}{\partial V} \right)_S$  should be negative i.e. the temperature should decrease with increasing volume under condition of constant entropy or adiabatic process. So an adiabatic expansion must result in a fall of temperature.

Again from Maxwell's thermodynamic relation, we have -

$$\left( \frac{\partial T}{\partial P} \right)_S = \left( \frac{\partial V}{\partial S} \right)_P$$

$$\Rightarrow \left( \frac{\partial T}{\partial P} \right)_S = T \left( \frac{\partial V}{\partial Q} \right)_P$$

Since an increase in quantity of heat at constant P always results in increase in volume. So the -



term  $\left(\frac{\partial V}{\partial Q}\right)_p$  is positive and  $\left(\frac{\partial T}{\partial P}\right)_s$  must be positive.

i.e. temperature must increase with an increase in  $p$  under condition of constant entropy or adiabatic process. So as adiabatic compression always results an increase in temperature.

16. Joule-Thomson expansion: When a gas at constant high pressure is forced through a porous plug to a region of constant low pressure, the temperature of the escaping gas changes, this is called Joule-Thomson expansion.

During Joule-Thomson expansion enthalpy 'H' of the gas remains constant.

$$H = U + PV = \text{constant}$$

$$\therefore dH = dU + PdV + VdP = 0$$

$$\text{But, } dQ = dU + PdV$$

$$\therefore dQ + VdP = 0$$

$$\Rightarrow Tds + VdP = 0 \quad \text{--- (1)} \quad \left[ \begin{array}{l} \text{using 1st and} \\ \text{2nd law} \end{array} \right]$$

If we make entropy 's' as a function of two independent variables T and P then the change in entropy can be expressed as -

$$ds = \left(\frac{\partial s}{\partial T}\right)_p dT + \left(\frac{\partial s}{\partial P}\right)_T dP$$

$$\Rightarrow Tds = T \left(\frac{\partial s}{\partial T}\right)_p dT + T \left(\frac{\partial s}{\partial P}\right)_T dP$$

$\therefore$  Eq<sup>n</sup> (1) becomes  $\Rightarrow$

$$T \left(\frac{\partial s}{\partial T}\right)_p dT + T \left(\frac{\partial s}{\partial P}\right)_T dP + VdP = 0 \quad \text{--- (2)}$$

Now,  $T \left(\frac{\partial s}{\partial T}\right)_p = \left(\frac{\partial Q}{\partial T}\right)_p = C_p$  ; the specific heat at constant pressure.



Also from Maxwell's relation.

$$\left(\frac{\partial S}{\partial P}\right)_T = -\left(\frac{\partial V}{\partial T}\right)_P$$

∴ Eq<sup>n</sup> (2) becomes  $\Rightarrow$

$$C_p dT - T \left(\frac{\partial V}{\partial T}\right)_P dP + V dP = 0$$

$$\Rightarrow C_p dT = \left\{ T \left(\frac{\partial V}{\partial T}\right)_P - V \right\} dP$$

Joule-Thomson coefficient is given by -

$$\mu = \left(\frac{\partial T}{\partial P}\right)_H = \frac{1}{C_p} \left\{ T \left(\frac{\partial V}{\partial T}\right)_P - V \right\} \quad (3)$$

This expression gives the change in temperature  $T$  of a gas due to Joule-Thomson effect.

For a perfect gas the eq<sup>n</sup> of state is  $PV = RT$

Differentiating wrt 'T' keeping 'P' as constant we get  $\Rightarrow$

$$\left(\frac{\partial V}{\partial T}\right)_P = \frac{R}{P}$$

$$\therefore T \left(\frac{\partial V}{\partial T}\right)_P = \frac{RT}{P} = \frac{PV}{P} = V$$

∴ from eq<sup>n</sup> (3), we get  $\Rightarrow$

$$\boxed{\mu = 0}$$

So Joule-Thomson coefficient for a perfect gas is zero.

For a real gas the eq<sup>n</sup> of state is -

$$\left(P + \frac{a}{V^2}\right)(V-b) = RT$$

Differentiating wrt 'T' taking 'P' constant, we get  $\Rightarrow$

$\rightarrow$

$$\left(p + \frac{a}{V^2}\right) \left(\frac{\partial V}{\partial T}\right)_p - \left(\frac{2a}{V^3}\right) (V-b) \left(\frac{\partial V}{\partial T}\right)_p = R$$

$$\Rightarrow \left(\frac{\partial V}{\partial T}\right)_p = \frac{R}{\left(p + \frac{a}{V^2}\right) - \frac{2a}{V^3}(V-b)}$$

$$\Rightarrow \left(\frac{\partial V}{\partial T}\right)_p = \frac{R}{\frac{RT}{V-b} - \frac{2a}{V^3}(V-b)}$$

$$\Rightarrow \left(\frac{\partial V}{\partial T}\right)_p = \frac{R(V-b)}{RT - \frac{2a}{V^3}(V-b)^2}$$

$\because V \gg b$  so we can neglect  $b$  and can write  $V^2$  in place of  $(V-b)^2$ .

$$\therefore \left(\frac{\partial V}{\partial T}\right)_p = \frac{R(V-b)}{RT - \frac{2a}{V}}$$

$$\Rightarrow \left(\frac{\partial V}{\partial T}\right)_p = \frac{V-b}{T - \frac{2a}{VR}}$$

$$\therefore T \left(\frac{\partial V}{\partial T}\right)_p = \frac{T(V-b)}{T - \frac{2a}{VR}} = \frac{V-b}{1 - \frac{2a}{RTV}}$$

$$\Rightarrow T \left(\frac{\partial V}{\partial T}\right)_p = (V-b) \left(1 - \frac{2a}{RTV}\right)^{-1}$$

$$\Rightarrow T \left(\frac{\partial V}{\partial T}\right)_p = (V-b) \left(1 + \frac{2a}{RTV}\right)$$

$$\Rightarrow T \left(\frac{\partial V}{\partial T}\right)_p = V-b + \frac{2a}{RT} - \frac{2ab}{RTV}$$

$$\Rightarrow T \left(\frac{\partial V}{\partial T}\right)_p = V-b + \frac{2a}{RT}$$

Expanding binomially and neglecting higher order  
 $\left[ \frac{2ab}{RTV} \right]$  can be neglected since  $a$  and  $b$  very small

$$\Rightarrow T \left( \frac{\partial V}{\partial T} \right)_P - V = \frac{2a}{RT} - b$$

Substituting the value in eq<sup>n</sup> (3), we get  $\Rightarrow$

$$\boxed{\mu = \frac{1}{C_p} \left( \frac{2a}{RT} - b \right)}$$

This is the expression for Joule-Thomson coefficient for real gas.

On this expression it is clear that if  $\frac{2a}{RT} > b$  i.e.,  $T < \frac{2a}{Rb}$  then  $\mu = \left( \frac{\partial T}{\partial P} \right)_H$  is positive. Since  $\partial P$  is negative quantity so  $\partial T$  also should be negative hence the gas should be cool passing through the Porous plug.

Again,  $\frac{2a}{RT} < b$  and  $T > \frac{2a}{Rb}$  then  $\mu$  is negative so  $\partial T$  will be positive because  $\partial P$  is always negative thus the gas will be heated up on passing through Porous plug.

Now, if  $\frac{2a}{RT} = b$  i.e.  $T = \frac{2a}{Rb}$  then  $\mu = 0$  i.e. the gas passing through the Porous plug will show no change in temperature.

The temperature at which Joule-Thomson coefficient changes in sign is known as temperature of inversion

which is denoted by  $\boxed{T_i = \frac{2a}{Rb}}$ ,

=. ✓

Q. Show that for a homogeneous fluid  $C_p - C_v = T \left( \frac{\partial p}{\partial T} \right)_V \left( \frac{\partial v}{\partial T} \right)_P$  and hence prove that-

(i) For a perfect gas-  $C_p - C_v = R$

(ii) For a Vander Waal's gas-  $C_p - C_v = R \left( 1 + \frac{2a}{RTV} \right)$ .

↳ The specific heat at constant P and constant V are given by-

$$C_p = \left( \frac{\partial Q}{\partial T} \right)_P = T \left( \frac{\partial S}{\partial T} \right)_P \quad \text{--- (1)} \quad \left[ \because \partial Q = T \partial S \right]$$

$$C_v = \left( \frac{\partial Q}{\partial T} \right)_V = T \left( \frac{\partial S}{\partial T} \right)_V \quad \text{--- (2)}$$

If entropy has the function of 'T' and 'V' then-

$$dS = \left( \frac{\partial S}{\partial T} \right)_V dT + \left( \frac{\partial S}{\partial V} \right)_T dV$$

Differentiating the above eq<sup>n</sup> at constant 'P' and multiply it with 'T', we get  $\Rightarrow$

$$T \left( \frac{\partial S}{\partial T} \right)_P = T \left( \frac{\partial S}{\partial T} \right)_V + T \left( \frac{\partial S}{\partial V} \right)_T \left( \frac{\partial V}{\partial T} \right)_P$$

$$\Rightarrow C_p = C_v + T \left( \frac{\partial S}{\partial V} \right)_T \left( \frac{\partial V}{\partial T} \right)_P \quad \text{--- (3)} \quad \left\{ \begin{array}{l} \text{using eq. (1)} \\ \text{and eq. (2)} \end{array} \right\}$$

using Maxwell's relation, we have-

$$\left( \frac{\partial S}{\partial V} \right)_T = \left( \frac{\partial P}{\partial T} \right)_V$$

So, eq<sup>n</sup> (3) becomes  $\Rightarrow$

$$C_p - C_v = T \left( \frac{\partial P}{\partial T} \right)_V \left( \frac{\partial V}{\partial T} \right)_P \quad \text{--- (4)}$$

(i) For a perfect gas.  $PV = RT$ ,

→

Differentiating 'P' wrt 'T' at constant 'V', we get  $\Rightarrow$

$$\left(\frac{\partial P}{\partial T}\right)_V = \frac{R}{V}$$

Again differentiating 'V' wrt 'T' at constant 'P'  $\Rightarrow$

$$\left(\frac{\partial V}{\partial T}\right)_P = \frac{R}{P}$$

Substituting the values in eq<sup>n</sup> (4), we get  $\Rightarrow$

$$C_p - C_v = T \left(\frac{R}{V}\right) \left(\frac{R}{P}\right)$$

$$\Rightarrow C_p - C_v = \frac{R(RT)}{PV}$$

$$\Rightarrow \boxed{C_p - C_v = R} \quad \left[ \because RT = PV \right]$$

(ii) For Vanderwaal's gas, we have-

$$\left(P + \frac{a}{V^2}\right)(V-b) = RT \Rightarrow P + \frac{a}{V^2} = \frac{RT}{V-b}$$

Differentiating wrt 'T' at constant 'V', we get  $\Rightarrow$

$$\left(\frac{\partial P}{\partial T}\right)_V = \frac{R}{V-b}$$

Again, differentiating wrt 'T' at constant 'P', we get  $\Rightarrow$

$$\frac{-2a}{V^3} \left(\frac{\partial V}{\partial T}\right)_P = \frac{R}{V-b} - \frac{RT}{(V-b)^2} \left(\frac{\partial V}{\partial T}\right)_P$$

$$\Rightarrow \left\{ \frac{RT}{(V-b)^2} - \frac{2a}{V^3} \right\} \left(\frac{\partial V}{\partial T}\right)_P = \frac{R}{V-b}$$

$$\Rightarrow \left(\frac{\partial V}{\partial T}\right)_P = \frac{\frac{R}{V-b}}{\left\{ \frac{RT}{(V-b)^2} - \frac{2a}{V^3} \right\}}$$

substituting the values of  $\left(\frac{\partial P}{\partial T}\right)_V$  and  $\left(\frac{\partial V}{\partial T}\right)_P$  in eq<sup>n</sup>.

(4), we get  $\Rightarrow$

$$C_p - C_v = T \left( \frac{R}{V-b} \right) \frac{\frac{R}{V-b}}{\left\{ \frac{RT}{(V-b)^2} - \frac{2a}{V^3} \right\}}$$

$$\Rightarrow C_p - C_v = \frac{T \frac{R^2}{(V-b)^2}}{\frac{RT}{(V-b)^2} - \frac{2a}{V^3}}$$

Dividing numerator and denominator by  $\frac{RT}{(V-b)^2}$

$$\Rightarrow C_p - C_v = \frac{R}{1 - \frac{2a(V-b)^2}{RTV^3}}$$

$$\Rightarrow C_p - C_v = \frac{R}{1 - \frac{2aV^2}{RTV^3}} \quad \left[ \because b \ll V \right]$$

$$\Rightarrow C_p - C_v = \frac{R}{1 - \frac{2a}{RTV}}$$

$$\Rightarrow C_p - C_v = R \left( 1 - \frac{2a}{RTV} \right)^{-1}$$

$$\Rightarrow C_p - C_v = R \left( 1 + \frac{2a}{RTV} \right)$$

Expanding binomially and neglecting higher order.

✓ Phase: A phase is defined as the system which is homogeneous having defined boundaries.

A substance usually state either in solid liquid or in gaseous state, each of these state are called phase.

✓ Phase Transition: The process in which the thermodynamic system changes from one state to another with different physical properties is called phase transition.

✓ First Order transition: The phase transition in which temperature and pressure remains constant while the entropy and vol.<sup>m</sup> changes and also the first order derivatives of Gibb's function changes discontinuously is known as first order transition.

Example: Melting, vaporization, sublimation.

✓ Clausius Clapeyron equation of first order transition:

Let us consider 1 mole of a substance undergoes a change from phase  $i$  to phase  $f$ .

Now, from 1<sup>st</sup> Tds equation, we have  $\Rightarrow$

$$Tds = C_p dT + T \left( \frac{\partial P}{\partial T} \right)_V dV \quad \text{--- (1)}$$

Assuming that various  $P$  and  $T$  at which phase transition occurs obeys a relation where  $P$  is function of  $T$  only (independent of  $V$ ).

$$\therefore \left( \frac{\partial P}{\partial T} \right)_V = \frac{dP}{dT}$$

Again for first order transition -

$$dT = 0 \quad \text{and} \quad C_p = \infty \quad (\text{undefined}),$$

so, eq<sup>n</sup> (1) becomes  $\Rightarrow$

$$T(S_f - S_i) = T \frac{dP}{dT} (V_f - V_i)$$

and the left hand side of the equation is the latent heat per mole which is represented by-

$$L = T \frac{dP}{dT} (V_f - V_i)$$

$$\Rightarrow \boxed{\frac{dP}{dT} = \frac{L}{T(V_f - V_i)}}$$

which is Clausius Clapeyron's equation.

### Second Order phase transition:

The transition in which there is no change of entropy and volume but its discontinuity appear in specific heat and constant P and isobaric vol.<sup>m</sup> expansion. i.e., the first order derivative of Gibbs function are continuous but second order derivative show discontinuous state is known as 2nd order phase transition.

eg: The transition of normal He (He I) to superfluid (He II).

### Ehrenfest Equation of 2nd order phase transition:

In a second order phase transition the vol.<sup>m</sup> and entropy remains constant. The constancy of entropy is represented by -  $S_1 = S_2$  — (1). ; at temp. T and pressure P

where, the two phases are represented by 1 and 2 as the temperature is raised infinitesimally from T to  $(T + dT)$  and pressure from P. to  $(P + dP)$

then -  $S_1 + dS_1 = S_2 + dS_2$  — (2)

So, from eq<sup>n</sup>(1) and eq<sup>n</sup>(2); we get  $\Rightarrow$

$$dS_1 = dS_2 \quad \text{--- (3)}$$

Now, expressing entropy as a function of T and P, we get  $\Rightarrow$

$$dS = \left(\frac{\partial S}{\partial T}\right)_P dT + \left(\frac{\partial S}{\partial P}\right)_T dP$$

$$\Rightarrow dS = \left(\frac{\partial S}{\partial T}\right)_P dT - \left(\frac{\partial V}{\partial T}\right)_P dP \quad \left\{ \text{using Maxwell's relation} \right\}$$

$$\Rightarrow dS = \frac{C_p}{T} dT - V\alpha dP \quad \text{--- (2)} \quad ; \quad \left[ \alpha = \frac{1}{V} \left(\frac{\partial V}{\partial T}\right)_P \right]$$

Where,  $C_p = T \left(\frac{\partial S}{\partial T}\right)_P$  is the specific heat at constant pressure is the isobaric vol.<sup>m</sup> expansim.

Since vol.<sup>m</sup>  $V$  is the same for both the phases.

$$\therefore dS_1 = \left(\frac{C_{p1}}{T}\right) dT - V\alpha_1 dP$$

$$\text{and } dS_2 = \left(\frac{C_{p2}}{T}\right) dT - V\alpha_2 dP$$

using eq<sup>n</sup>(3), we can write  $\Rightarrow$

$$\left(\frac{C_{p1}}{T}\right) dT - V\alpha_1 dP = \left(\frac{C_{p2}}{T}\right) dT - V\alpha_2 dP$$

$$\Rightarrow \left(\frac{C_{p1} - C_{p2}}{T}\right) dT = (\alpha_1 - \alpha_2) V dP$$

$$\Rightarrow \boxed{\left(\frac{dP}{dT}\right)_S = \frac{C_{p1} - C_{p2}}{(\alpha_1 - \alpha_2) TV}} \quad \text{--- (4)}$$

Again, starting from the combination of vol.<sup>m</sup> i.e.  $V_1 = V_2$ , we get for infinitesimally small -

$$dV_1 = dV_2 \quad \text{--- (5)}$$

Now expressing  $V$  as a function of  $T$  and  $P$  we get  $\Rightarrow$

$$dV = \left( \frac{\partial V}{\partial T} \right)_P dT + \left( \frac{\partial V}{\partial P} \right)_T dP$$

$$\Rightarrow dV = \alpha V dT - V K_T dP \quad \text{--- (7)}$$

Here,  $K_T = -\frac{1}{V} \left( \frac{\partial V}{\partial P} \right)_T$  is the bulk modulus of elasticity at constant temperature using (8) and (7) we can write  $\Rightarrow$

$$\alpha_1 V dT - V K_{T_1} dP = \alpha_2 V dT - V K_{T_2} dP$$

$$\Rightarrow (\alpha_1 - \alpha_2) V dT = V (K_{T_1} - K_{T_2}) dP$$

$$\Rightarrow \boxed{\left( \frac{dP}{dT} \right)_V = \frac{\alpha_1 - \alpha_2}{K_{T_1} - K_{T_2}}} \quad \text{--- (8)}$$

Eq<sup>n</sup> (8) and (8) are known as Ehrenfest's eq<sup>n</sup> of 2<sup>nd</sup> order transition.  $\checkmark$

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